

Release Note

Release Date : Oct. 07, 2021

Product Ver. : Civil 2022 (v1.1)



DESIGN OF CIVIL STRUCTURES

ntegrated Solution System for Bridge and givil Engineering

Enhancements

- 1. UK CS 454 Bridge Assessment for Steel Composite Girder
- 2. UK High-Speed Train Loads Database for Train Load Generator
- 3. Train Load Generator Time Forcing Function Improvement
- 4. AS 5100.5:17 Update for midas GSD
- 5. Italy NTC 2018 RS function
- 6. Auto-generation of Beam Section Temperature Loads (AASHTO, Eurocode, Australia)
- 7. Load Rating LRFR 2019 Update to AASHTO MBE 3rd edition
- 8. Traffic Load AK, N11 Update to Russia Standard
- 9. Longitudinal Stiffener Input Measured from Bottom of Steel Composite Girder



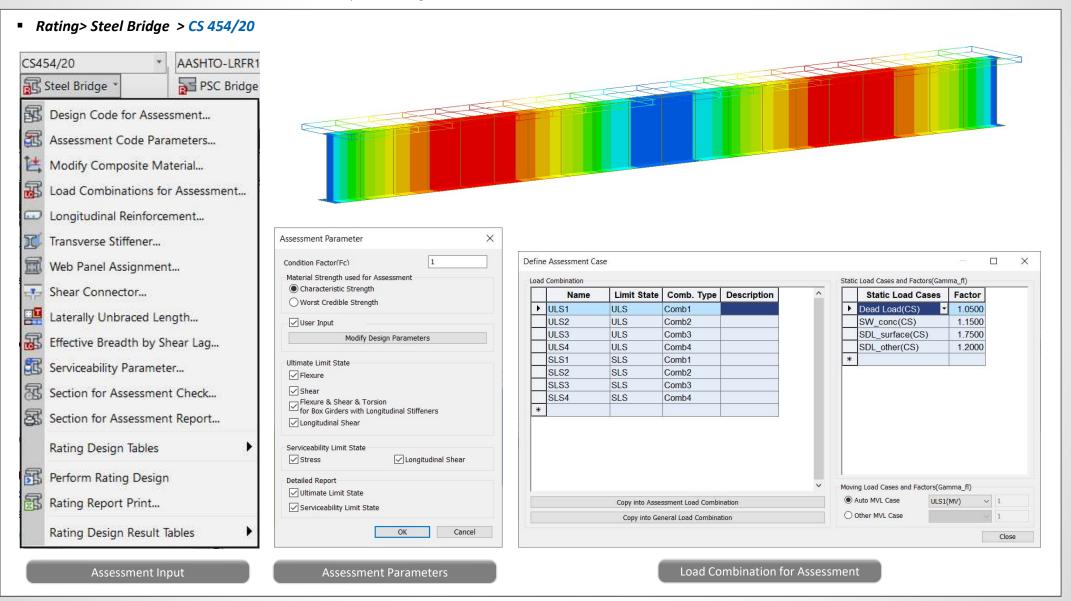
1. UK CS 454 Bridge Assessment for Steel Composite Girder

Steel composite girder assessment to CS 454 and CS 457 has been added.



1. UK CS 454 Bridge Assessment for Steel Composite Girder

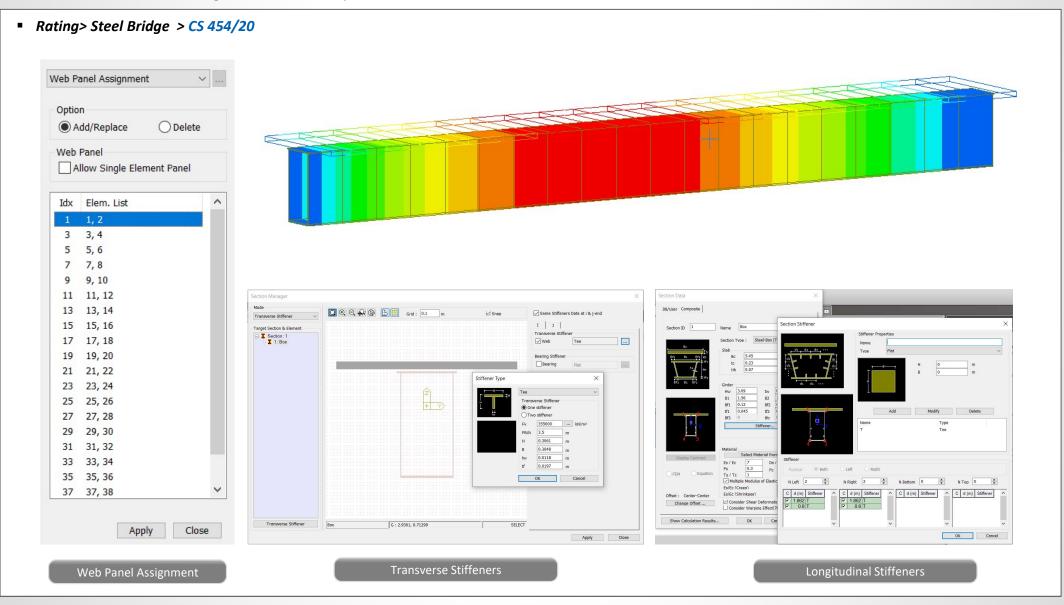
- Level 1 assessment can be performed now for the steel composite girders in midas Civil.
- Assessment load combinations can be defined to obtain output for strength & service limit states.





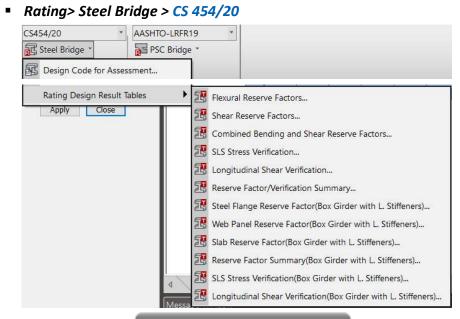
1. UK CS 454 Bridge Assessment for Steel Composite Girder

- · Assessment can be performed depending on section types such as plate girders and box girders. (Note: Box girder assessment will not be included in this release.)
- Stiffeners in the transverse and longitudinal direction, web panels, shear connectors can be defined.



1. UK CS 454 Bridge Assessment for Steel Composite Girder

- Assessment results can be viewed in tabular format in midas Civil itself and these can be exported to excel file as well.
- Both summary ands detailed report are provided for the bending, shear, combined bending and shear, longitudinal shear checks and service limit state.



Assessment Result Tables

| | Element | Part | | F | Ratin | ng Case | | Comp./ Tens. | Sig_y (N/mn | | Sig_f_SV (N/mm²) | | V Sig_f_D 1 ²) (N/mm ² | | Sig_f_S (N/mm ² | | | Ps | | Psi* | Che | ck | |
|---|---------|-------|----|-----|-------|---------|------|-----------------|----------------|-----|-----------------------|-------|--|---------------|-------------------------------|----------------------|----------------|----------------------|-----|----------------|---------|---------|------|
| • | 10 | I[10] | UL | .S1 | Fxx | (Max) | | 74 74 | - 0.00 | 00 | 0.0000 | 20781 | 05 0.000 | 0.000 | 0.000 | 0.000 | 0.00 | 00 | - | | - NG | | |
| | 10 | I[10] | UL | S1 | Fyy | (Max) | | | - 7.63 | 13 | 0.0000 | 0.00 | 6.592 | 9 0.000 | 0.000 | 0.000 | 00 | - 1000 | 000 | 10000 | 00 OK | | |
| | 10 | I[10] | UL | S1 | Fyy | (Min) | | | - 7.63 | 13 | 0.0000 | 0.00 | 00 6.592 | 9 0.000 | 0.000 | 0.000 | 00 | - 1000 | 000 | 10000 | 00 OK | | |
| | 10 | I[10] | UL | S1 | Fzz | (Max) | | | - 7.63 | 13 | -28.5044 | 0.00 | 00 -23.639 | 2 0.0000 | 4.781 | 3 0.000 | 00 | - 1000 | 000 | 10000 | 00 OK | | |
| | 10 | I[10] | UL | S1 | - | 78.4° 5 | | 1 | 7.00 | 40 | 00 7004 | 0.00 | 00.000 | | | | 1 | 4000 | 000 | 10000 | | | T |
| | 10 | I[10] | UL | S' | | Element | Pa | rt Sectio | n Type | | Rating Cas | e | Load Effect | RA* (kN⋅m) | S* (kN⋅m) | SD* (kN⋅m) | SST* (kN·m) | SA* (kN·m) | 1 | A | Psi | Psi* | Chec |
| | 10 | I[10] | UL | S' | | | | | | | 100 | | | | 1 | 1 A | | | | | | | |
| | 10 | I[10] | UL | S' | • | | |] Comp | | | _Fxx(Max) | | Negative | 7713.604 | 0.0000 | -393.340 | 0.0000 | -393.340 | | | 1000000 | 1000000 | - |
| | | I[10] | UL | | | | |] Comp | | | _Fxx(Min) | | Negative | 7713.604 | 0.0000 | -393.340 | 0.0000 | -393.340 | | | 1000000 | 1000000 | |
| | 10 | I[10] | UL | S' | | | |] Comp | | | _Fyy(Max) | | Negative | 7713.604 | 0.0000 | -393.340 | 0.0000 | -393.340 | | | 1000000 | 1000000 | |
| _ | 10 | I[10] | UL | S'- | | | | Comp Comp | | | _Fyy(Min) | | Negative | 7713.604 | 0.0000 | -393.340 -393.340 | 0.0000 | -393.340 -3148.27 | | 6105 1 4501 | 1000000 | 1000000 | OK |
| | | | | H | _ | | J[11 | Comp Comp | | | _Fzz(Max) Fzz(Min) | | Negative Negative | 7713.604 | 0.0000 | -393.340 | 0.0000 | -3140.27 | | | 1000000 | 1000000 | - |
| | | | | H | _ | | | 1 Comp | | | Mxx(Max | | Negative | 7713.604 | -1279.73 | -393.340 | -1664.86 | -2058.20 | | 7477 | 1000000 | | OK |
| | | | | H | | | | Comp | | | Mxx(Min) | | Negative | 7713.604 | -1279.73 | -393.340 | -1664.86 | -2058.20 | | 7477 | | | OK |
| | | | | h | | | | 1 Comp | | | Myy(Max | | Negative | 7713.604 | 0.0000 | -393,340 | 0.0000 | -393.340 | | | 1000000 | 1000000 | |
| | | | | h | | | | 1 Comp | | | Myy(Min) | | Negative | 7640.440 | -2449.06 | -393.340 | -2998.06 | -3391.40 | | 2529 | - | - | OK |
| | | | | h | | 10 | J[11 |] Comp | act U | LS1 | Mzz(Max |) | Negative | 7713.604 | 0.0000 | -393.340 | 0.0000 | -393.340 | 19. | 6105 1 | 1000000 | 1000000 | OK |
| | | | | | | 10 | J[11 | 1 Comp | act U | LS1 | Mzz(Min) | | Negative | 7713.604 | 0.0000 | -393.340 | 0.0000 | -393.340 | 19. | 6105 1 | 1000000 | 1000000 | OK |

Tabular Output in midas Civil

| Desig | gn (| Condit | ion | | | | | | | | | | | | | | | | | | | |
|----------|------|------------------------|-------------------|-------------------------|------------------------|--------------|------------|------------------------------------|---------------------|-------------------------|-----------------------|---------------------------------------|-------------------------|------------------|-------|---------------------------|------------------------|-----|--------|-----|----|-------|
| [| Desi | gn code | | Elemen | t Par | t(Node) | | | | | | | | | | | | | | | | |
| | CS4 | 154/20 | | 8 | | I(8) | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | | |
| Asse | ssm | ent fa | ctors | | | | | | | | | | | | | | | | | | | |
| The f | ollo | wing f | actors, | as in C | s 454, | have be | een use | d to d | ompa | re re | sults | of di | ffere | nt | | | | | | | | |
| confi | gur | ations | and co | mbina | tions. | | | .1 .1 | | 1 | | TT | | | | - | | | | | | |
| - A | dec | uacy fa | ctor: | | | 3. | Flexur | | serve | - | | | | | - | | | | _ | | | |
| | | | | م * | | | t | nen | Load | | ₹ _a * | S* | | S _D * | | S _{ST} * | S _a * | | A | Ψ | ψ* | Chec |
| | | | $A = \frac{1}{2}$ | $\frac{R_a}{C^*}$ | | | Case | 2 | Effect | (kľ | v.m) | (kN.r | n) (| (kN.m) | (k | (N.m) | (kN.r | m) | | | | |
| | | | | ³ a | 0.00 | | ULS1_Fxx | Max) N | Vegativ | e 781 | 8.638 | 0.00 | 0 -3 | 393.340 | 0 | 0.000 | -393.3 | 40 | 19.878 | - | - | ОК |
| 1 | | | | | | | ULS1_Fxx | (Min) N | Vegativ | e 781 | 8.638 | 0.00 | 0 -3 | 393.340 | 0 | 0.000 | -393.3 | 40 | 19.878 | 3-3 | - | ОК |
| • S | pec | ial Vehi | cle rese | erve fact | or v 4. | Shear R | eserve | Facto | ors | | | | | | | | | | 878 | - | - | ОК |
| | | $\Psi = \frac{1}{2}$ | $R_{a}^{*} - ($ | $S_{D}^{*} + S_{C}^{*}$ | (s_T) | Assessm | en Ra | | S* | SD | * | S _{ST} * | | S _a * | | Ψ | W * | | 878 | - | - | ОК |
| | | • | | S* | | t Case | (kN | 1) | (kN) | (kN | V) | (kN) | () | kN) | A | Ψ | Ψ* | Che | ck | - | - | ок |
| | | | | | | ULS1_Fxx(M | ax) - | | - | - | | | | - | - | - | - | - | 578 | - | - | ОК |
| • S | epc | ial Vehi | cle rese | erve fact | orv | ULS1_Fxx(N | lin) 7720. | 152 (| 0.000 | 201. | 277 | 0.000 | 201 | 1.277 3 | 8.356 | - | - | OI | | | | OK |
| | | , | 5 Cor | nhined | Bendi | ng and s | Shear P | osory | e Fact | ore | | | | | | | | | | | | |
| | | 2 | | essmen | Mp | M, | Vp | V, | | | V | | | V _{DL} | | M | V | | | | | |
| | | | | t | (kN.m) | (kN.m) | (kN) | (kN | | M _{sv} N.m) | V _s (kN | 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | M _{DL} N.m) | (kN) | | M _{st} (kN.m) | V _{S1} (kN | | Α | Ψ | Ψ* | Check |
| Whe | re: | | | Fxx(Max) | | 6769.383 | 7720.152 | | | .000 | 0.00 | | 2.941 | | | 0.000 | 0.00 | _ | 0.058 | - | | ОК |
| R*- | | the as | | Fxx(Min) | | 6769.383 | 7720.152 | | | .000 | 0.00 | | 2.941 | | | 0.000 | 0.00 | | 0.058 | - | | OK |
| Cir | | | | | | | | + | |) | 0.00 | | 2.941 | - | + | 0.000 | 0.00 | | 0.058 | - | | OK |
| 5* 5* | - | essmen | | ar Verifi | | | | - | |) | 0.00 | | 2.941 | NG | - | 0.000 | 0.00 | | 0.058 | - | | OK |
| | | t | q (kN/m) | P _{im} (kN) | P _a (kN) | q, (kN/m) | q/q, | (q/q _r) _{lin} | _{nit} Cheo | k 69 | 1371. | | 2.941 | - | | 2754.934 | 1795.2 | | 0.465 | - | | OK |
| S | _ | Case L_Fxx(Max) | 0.032 | 125.000 | 82.642 | 0.248 | 0.065 | 1.000 | NG | 5 | 0.00 | | 2.941 | | | 0.000 | 0.00 | | 0.058 | - | | ОК |
| 3 | ULS | 1_Fxx(Min) | - | - | 3-3 | - | - | - | - | 37 | 402. | 45 -32 | 2.941 | NG | 1- | 1664.865 | 823.6 | 72 | 0.304 | - | | ОК |
| | ULS | L_Fyy(Max) | 0.032 | 125.000 | 82.642 | 0.248 | 0.065 | 1.000 | NG | 37 | 402.1 | 45 -32 | 2.941 | NG | - | 1664.865 | 823.6 | 72 | 0.304 | - | | ОК |
| | ULS | 1_Fyy(Min) | 0.032 | 125.000 | 82.642 | 0.248 | 0.065 | 1.000 | NG | 5 | 0.00 | 00 -32 | 2.941 | NG | T | 0.000 | 0.00 | 00 | 0.058 | - | | ОК |
| | ULS | 1_Fzz(Max) | 0.578 | 125.000 | 82.642 | 0.248 | 1.166 | 1.000 | NG | 66 | 1174. | 535 -32 | 2.941 | NG | - | 2998.067 | 1470.5 | 545 | 0.501 | - | | ОК |
| | | 1_Fzz(Min) | 0.255 | 125.000 | 82.642 | 0.248 | 0.513 | 1.000 | NG | | 0.00 | 0 -32 | 2.941 | NG | 1 | 0.000 | 0.00 | 00 | 0.058 | - | | ОК |
| | | _Mox[Max] | 0.351 | 125.000 | 82.642 | 0.248 | 0.708 | 1.000 | NG | ······ | 0.00 | | 2.941 | | | 0.000 | 0.00 | | 0.058 | - | | OK |
| - | | _Mxx(Min) | 0.077 | 125.000 | 82.642 82.642 | 0.248 | 0.156 | 1.000 | NG | | | | | | - | | | | | | | |
| | 0151 | _Myy(Max) _Myy(Min) | 0.077 | 125.000 125.000 | 82.642 | 0.248 | 0.155 | 1.000 | NG | | | | | | | | | | | | | |
| | ULS1 | | | | | | | 1.000 | | | | | | | | | | | | | | |
| | | _Mzz(Max) | 0.032 | 125.000 | 82.642 | 0.248 | 0.065 | 1.000 | NG | | | | | | | | | | | | | |

Excel Report Output

2. UK High-Speed Train Loads Database for Train Load Generator

- UK high-speed train loads database are available in the Train Load Generator.
- UK Vehicle data is provided as per the clause of UK HS2.

Load > Dynamic Loads > Time History Analysis Data > Train Load Generator > Vehicle Code - UK

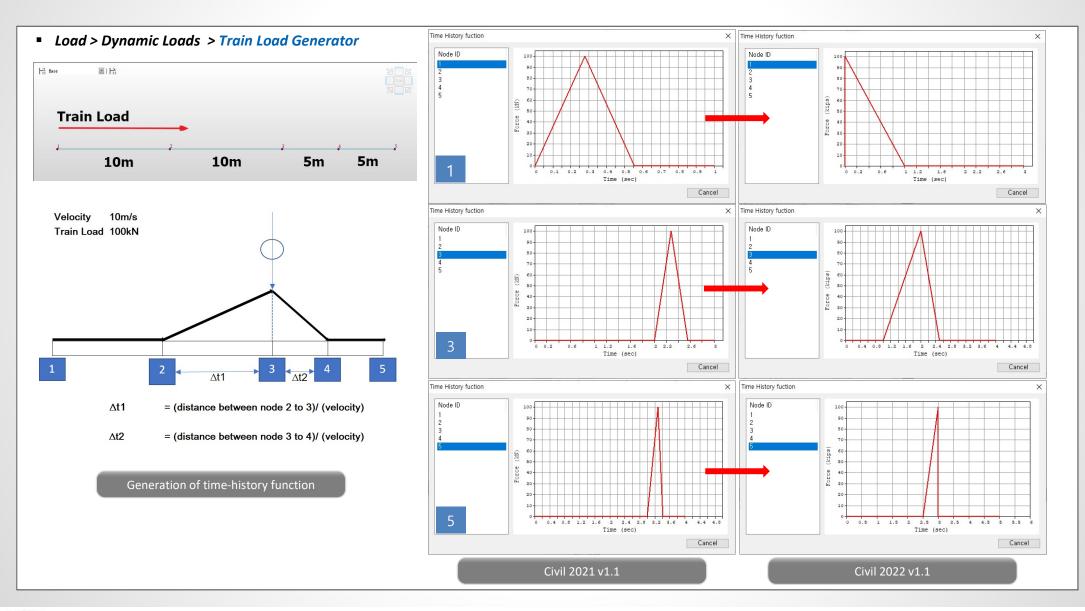
| Train Load Generator | | | × |
|---------------------------------|--------|----------------|---------------|
| Define Tracks | No | Length(m) | Force(kN) |
| | | 0,000 | 177,000 |
| 0,0,0 | m 2 | 2,800 | 177,000 |
| 100,0,0 | m 3 | 8,200 2,800 | 177,000 |
| | 4 | 4,500 | 111,000 |
| Operations | 6 | 13,140 | 215.000 |
| Add Insert Dele | | 13,100 | 209,000 |
| insert Der | 8 | 13,100 | 216.000 |
| | 1.9 | 13,100 | 222,000 |
| No Node Distance(n | n) 10 | 13.100 | 222.000 |
| 1 128 | 0 11 | 13,100 | 214,000 |
| 2 129 | 5 12 | 13,100 | 214,000 |
| | 5 13 | 13,100 | 222,000 |
| 3 130 | | 13,100 | 222,000 |
| 4 131 | 5 15 | 13,100 | 222,000 |
| 5 132 | 5 16 | 13,100 | 228,000 |
| Dynamic Load Case test | ~ 17 | 13,140 | 117,000 |
| - | 18 | 4,500 | 177,000 |
| Name UK | 19 | 2,800 | 177,000 |
| Vehicle Code UK | 20 | 8,200 2,800 | 177,000 |
| Vehicle Type Articulated Single | | 2,000 | 177,000 |
| Number of Wheels 21 | | | |
| Train Velocity 200 | km/h | | |
| | NIT/TI | | |
| Scaling | | | - |
| Scale Factor | | | |
| | | | |
| O Max, Value | | | |
| Time | | | |
| Start Time 0 🔹 | sec | Add Modify | Delete Insert |
| Load Direction -Z | ~ | Length 0 | Force 0 |
| Open Save As Import | . Sho | w Graph | OK Cancel |

Train Load Generator

| Dynamic Load Case | test v | |
|--|---|--|
| Name | | |
| Vehicle Code | UK ~ | |
| Vehicle Type | Articulated Single 🗸 | |
| Number of Wheels Train Velocity Scaling Scale Factor [1 O Max, Value [0] | Articulated Single Axle Articulated Double Deck 11 Articulated Double Deck 10 Articulated Distributed Conventional Current Conventional Omni Conventional Future 1 Conventional Future 2 Conventional Segmented 28m | |
| | Vehicle Code & Type | |
| | | |
| the transmit | Dynamic Nodal Loads | |

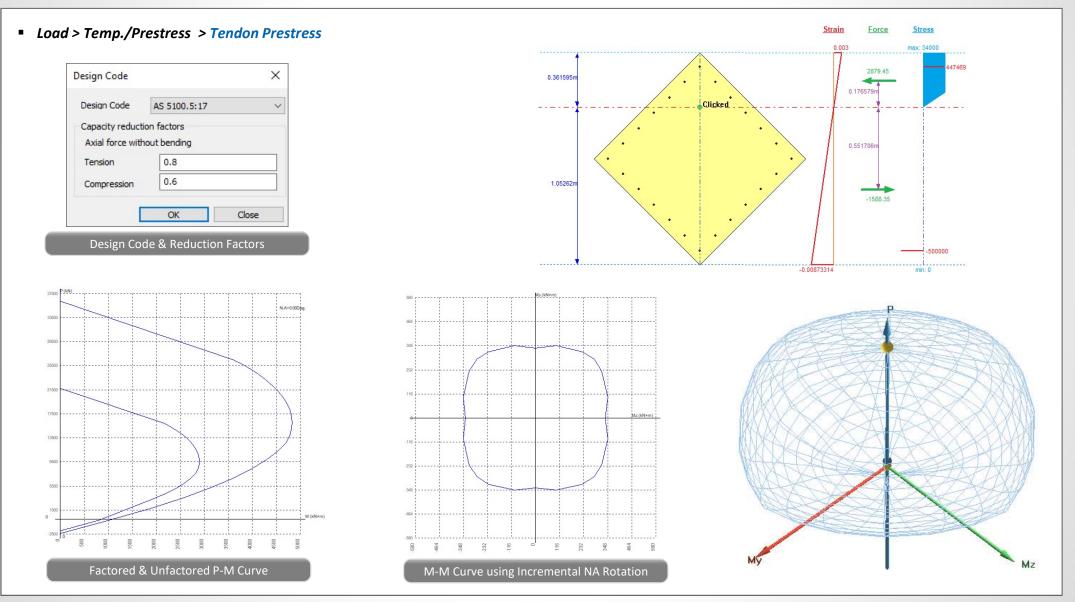
3. Train Load Generator Time Forcing Function Improvement

- Time-history function is improved for the nodes which have different distances between nodes.
- Time-history function is also improved for the first node and the last node of the track.



4. AS 5100.5:17 Update for midas GSD

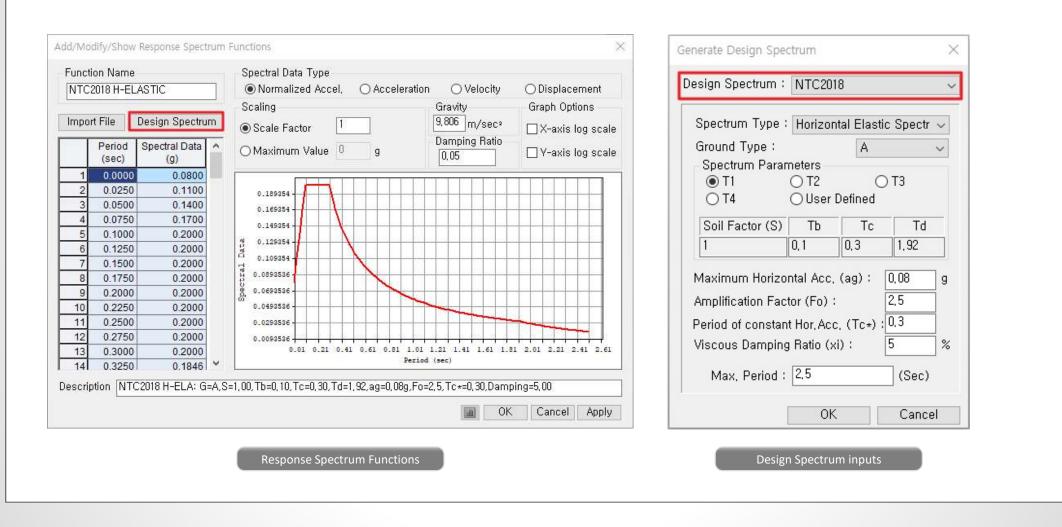
- Factored & unfactored P-M curve, M-M curve and stress contours based on AS 5100.5:17 can now be generated in midas GSD.
- Accurate M-M curve calculations with incremental NA rotation is adopted as it could be used for any section shape. This is preferred over traditional empirical approach in the code.



5. Response Spectrum Function: Italy NTC 2018

Response spectrum function as per Italy NTC 2018 has been added.

Load > Dynamic Loads > RS Functions



6. Auto-generation of Beam Section Temperature Loads (AASHTO, Eurocode, Australia)

- Auto definition of the temperature gradient for PSC and Steel composite girders as per AASHTO LRFD 2020.
- Applicable for sections defined from PSC, Composite tab (not applicable for SPC and Value type sections).
- Load > Temp/Prestress> Beam Section Temperature > AASHTO LRFD 2020

| | e Name | ~ | |
|---|----------|--------------------|--------------------|
| Load Gro | up Name | | |
| Default | | ~ | |
| Options | | | |
| Add | OReplace | ODe | elete |
| | | | |
| Top ↓ <u><u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u></u></u> | I | <u><u>H1,</u>T</u> | H2,T2 11 tom |
| | | | |

| Define Code AASHTO LRFD 2020 V Section Type PSC Temperature Grescel Composite Positive Negative T1 54 [T] T2 14 [T] T3 5 [T] A Auto User 12 in | Depth of super-structure T_1 R_1 T_2 T_2 T_3 |
|---|--|
| | OK Cancel |

6. Auto-generation of Beam Section Temperature Loads (AASHTO, Eurocode, Australia)

- Auto definition of the temperature gradient for PSC and Steel composite girders as per Eurocode.
- Applicable for section defined from PSC, Composite tab (not applicable for SPC and Value type sections).

Load > Temp/Prestress> Beam Section Temperature > Eurocode

| Load Case Na | me | | |
|--|-------------|---------|------------|
| | | ~ | |
| Load Group Na | ame | | |
| Default | | ~ | |
| Section Type | Replace | | |
| ◯ General | PSC/0 | Composi | te |
| Apply by Co | de Provisio | on | |
| Top ↓ <u><u><u></u><u></u><u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u></u></u></u> | | HITI | ⊒ 12,T2 |

| Depth of super- h h_2 ΔT_2 |
|---|
| h_3 ΔT_3 |
| $\begin{array}{rcl} h_1 &=& 0.3h & but &\leq 0.15m \\ h_2 &=& 0.3h & but &\geq 0.10m \end{array}$ |
| $h_3 = 0.3h$ but $\leq 0.25m$ $h_3 = 0.3h$ but $\geq 0.10m + 10m$ |
| surfacing depth in metres) (for thin slabs, h_3 is limited by $h - h_1 - h_2$) |
| h ΔT_1 ΔT_2 ΔT_3 |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ |
| |

Auto Option as per Code Provision

6. Auto-generation of Beam Section Temperature Loads (AASHTO, Eurocode, Australia)

- Auto definition of the temperature gradient for PSC and Steel composite girders as per AS 5100.
- Applicable for section defined from PSC, Composite tab (not applicable for SPC and Value type sections).

Load > Temp/Prestress> Beam Section Temperature > AS 5100

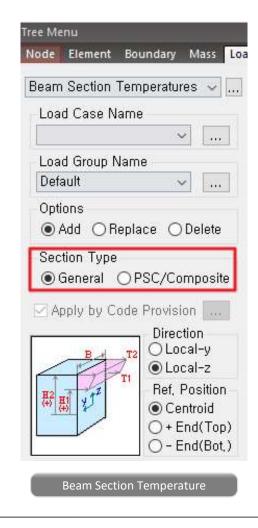
| | ame | ~ | | |
|------------------|---------|-------|-------|--|
| Load Group N | Vame | | | |
| Default | | ~ | | |
| Options | | | | |
| ● Add ○ | Replace | ODe | lete | |
| Apply by C | | | | |
| Тор | | | | |
| + H1,T1 H2,T2 | | | - | |
| - | - | H1,T1 | 12,T2 | |
| t | | Bott | om | |
| | | | | |

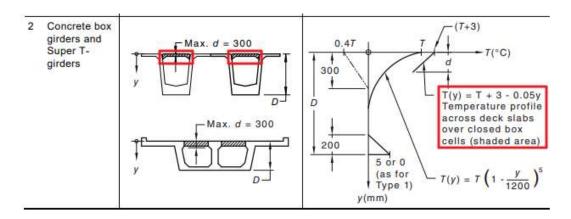
| Temperature G | ○ Negative | Deck concrete surface $0.4T$ T T $T(^{\circ}C)$ D $T(y) = T \left(1 - \frac{y}{1200}\right)^{5}$ |
|---------------|------------|---|
| | | Soffit y (mm) Soffit within 8m of ground 0 - over water |

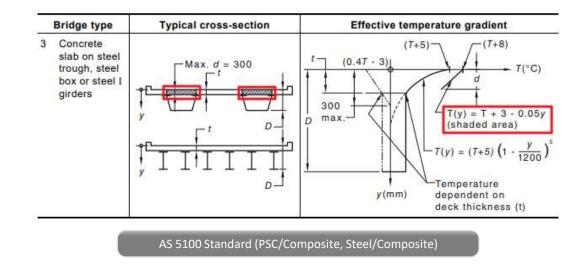
Auto Option as per Code Provision

6. Auto-generation of Beam Section Temperature Loads (AASHTO, Eurocode, Australia)

- The AS 5100 standard has different temperature distributions between the shaded area and other area of the top slab of the PSC sections, but in this function, the temperature distribution of other area is applied to the whole area of the top slab.
- It is recommended to use the General Section Type in Beam Section Temperatures to apply the temperature distribution of the shaded area.
- Load > Temp/Prestress > Beam Section Temperature > General Type







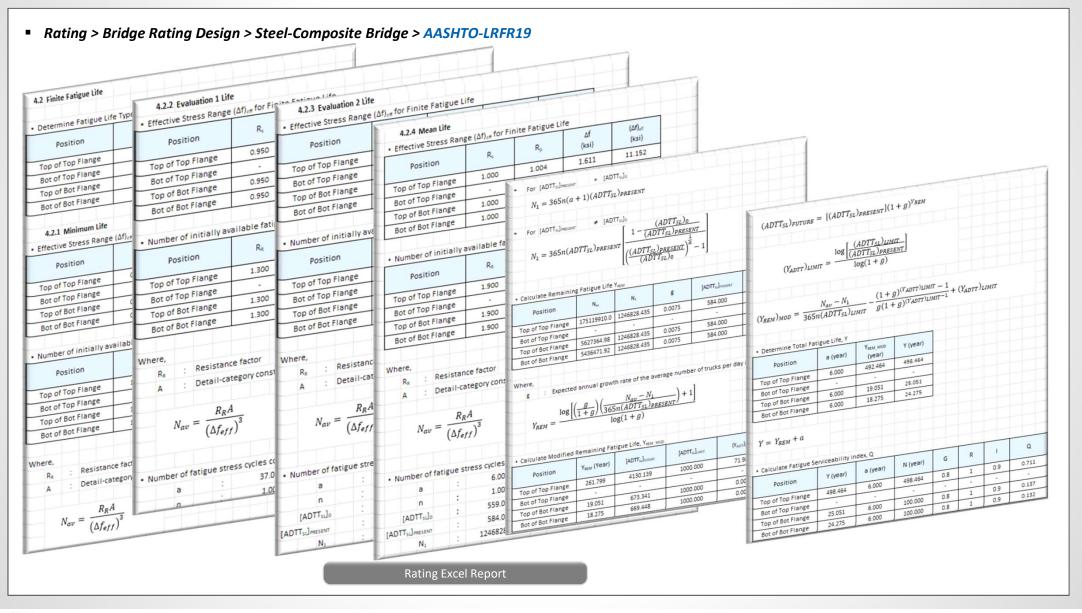
7. Load Rating LRFR 2019 Update to AASHTO MBE 3rd edition - Steel Composite Girder

- Service, Strength & Fatigue rating are available for steel composite girder based on AASHTO-LRFR19.
- Finite/Infinite life as well as serviceability index could be viewed in the software and the excel report could be referred to for detailed calculations.

| | | | Steel Bridge Load Rating Parameters X System factor 1 Update by Code | Tree Menu | Fatigue Parameter V |
|---|--|----------------|---|--|--------------------------------------|
| eel Bridge Load Rating Paramet | ers | × | Strength Limit State | Gen Steel Con SRC PSC CPG | Option |
| | | 1 | Strength Resistance Factor | | Add/Replace O Delete |
| System factor I Strength Limit State | | Update by Code | Resistance factor for yielding (Phi_y) 0.95 | Fatigue Parameter v | Gran, apare Oberen |
| Strength Limit State | | | Resistance factor for fracture(Phi_u) 0.8 | Fatigue Parameter 🗸 | Bally and anote (& 3) have the same |
| Resistance factor for yielding (| (Phi v) | 0.95 | Resistance factor for axial comp. (Phi_c) 0.9 Resistance factor for flexure (Phi_f) 1 | | Both end parts(i & j) have the same |
| Resistance factor for fracture(| | 0.8 | | Option | type |
| Resistance factor for axial com | | 0.9 | | Option Option | IJ |
| Resistance factor for flexure (F | Phi_f) | 1 | Resistance factor for shear connector(Phi_se) 0.85 Resistance factor for bearing(Phi_b) 1 | Add/Replace O Delete | |
| Resistance factor for shear (Phi | | 1 | | | Num.of Lanes, nL 0 |
| Resistance factor for shear cor | nnector(Phi_se) | 0.85 | Girder Type for Box/Tub Section | Both end parts(i & j) have the same | |
| Resistance factor for bearing(P | Phi_b) | 1 | ○ Single Box Sections | Both end parts(i & j) have the same type | vie rijresene |
| Girder Type for Box/Tub Section | 1 | | Consider St. Venant Torsion and Distortion Stresses | | (ADTTSL)Present 0 |
| O Single Box Sections | Multiple Box Section | ns | Option For Strength Limit State Appendix A6 for Negative Flexure Resistance in Web Compact | IJ | n(cycles) 0 |
| Consider St. Venant Torsion | | | / NonCompact Sections | | n(cycles) 0 |
| Option For Strength Limit State | | | ✓ Mn<=1.3RhMy in Positive Flexure and Compact Sections(6.10.7.1.2-3) | Category A 🗸 🗸 | Check Position Category |
| Appendix A6 for Negative Fl | | npact | Post-buckling Tension-field Action for Shear Resistance(6.10.9.3.2) | | checkrosition |
| / NonCompact Sections | | | | (ADTT)SL 0 | 🗹 Top of Top Flange 🛛 A 🗸 🗸 |
| Mn<=1.3RhMy in Positive Fl | | | ☑ Service Limit State | n(cycles) 0 | Bot. of Top Flange 🗛 🗸 |
| Post-buckling Tension-field A | Action for Shear Resistance(6 | .10.9.3.2) | Auto-Calculation Ouser Input | | |
| Service Limit State | | | Design Load | Warping Stress Range | 🗹 Top of Bot. Flange 🛛 🗛 🗸 🗸 |
| Limiting Stresses in Structural St | | | Compressive Stress 0 kN/m^2 | Auto Calculation | Bot. of Bot. Flange |
| Auto-Calculation | O User Input | | Tensile Stress 0 kW/m^2 | O User Input | |
| Design Load | 0 | 1211122 | Legal Load / Permit Load | O User Input | Marries Share Dance |
| Compressive Stress | | kN/m^2 | Compressive Stress 0 kN/m^2 | Top Flange | Warping Stress Range |
| Tensile Stress | 0 | kN/m^2 | Tensile Stress 0 kN/m^2 | | Auto Calculation |
| Legal Load / Permit Load | | | | 0 kN/m^2 | O User Input |
| Compressive Stress | | kN/m^2 | Fatigue Limit State | Bot, Flange | |
| Tensile Stress | 0 | kN/m^2 | | | Top of Top Flange |
| | | | Only infinite fatigue life | 0 kN/m^2 | 0 kN/m^2 |
| Fatique Limit State | | | Finite Fatigue Life Parameter | | PUL LE PLO PLOT |
| Application of Diagnostic Test Res | sult | | Current Age of the Detail, a 6 Year | | Bot, of Top Flange |
| Load Test Measurement | 🔘 Strain | Oisplacement | Expected Annual Growth Rate of ADTT_SL, g 0.0075 | | 0 kN/m^2 |
| | - | OK Count | Average Number of Truck per Day in a Single Lane | Apply Close | |
| | , | OK Cancel | (ADTT_SL)limit 1000 (ADTT_SL)0 559 | Close Close | Top of Bot. Flange |
| | | | | | 0 kN/m^2 |
| ad Rating Param | notore <u>Provi</u> | our Vorcione | Fatigue Serviceability Index | Fatigue Parameters – Previous Versions | |
| au Kaling Paran | ieters – Previ | ous versions | Load Path Factor, G 💿 0.80 🔿 0.90 🔿 1.00 | Faligue Parameters – Previous versions | Bot, of Bot, Flange |
| | | | Redundancy Factor, R O 0.90 💿 1.00 | | 0 kN/m^2 |
| | | | Important Factor, I 💿 0.90 🔿 0.95 🔿 1.00 | | 0 kN/m^2 |
| | | | | | |
| | | | Application of Diagnostic Test Result | | |
| | | | Load Test Measurement O Strain O Strain | | Apply Close |
| | | | | | Apply Close |
| | | | OK Cancel | | |

7. Load Rating LRFR 2019 Update to AASHTO MBE 3rd edition - Steel Composite Girder

- In earlier versions, just the classification whether the detail had infinite fatigue life or finite fatigue life was available.
- In Civil 2022, if the detail has finite fatigue life, then the minimum, evaluation I, evaluation II & mean fatigue life along with serviceability index are provided with detailed calculations.



7. Load Rating LRFR 2019 Update to AASHTO MBE 3rd edition - PSC Girder

- PSC/PSC Composite girders could now be rated based on AASHTO-LRFR19.
- In earlier versions, legal & permit load rating were combined. In newer version, these have been separated and stress ratio for reinforcement/tendon is now calculated for permit load rating.
- Tendon Primary load case should not be selected for the load combinations. It is automatically taken into account by the program.

| Define Rating Case X | Define Rating Case X | 3.2 Legal Load Rating 1) Rating Factor | | | Live Load | Rating | Factor | | |
|---|---|---|--|-----------------------------------|---|----------------------------|----------------------------|-----------------|----------|
| Static Load Combination | Static Load Combination | | (keil) | Dead Load Demand (ksi) | Demand (ksi) | 35.4 | 27 | | |
| Service Limit State O Strength Limit State | | Icom / Tens. | Capacity (ksi) | 4.144 | -0.564 | 0.55 | 52 | | 111 |
| | Service Limit State Strength Limit State | Lcom / Tens. | 24.132 | 4.144 | 1.862 | | | | |
| Load Type max min Load Cases | Load Type max min Load Cases | Legal Tens. | 5.171 | | | | | | |
| DC 1.00 1.00 * | DC 1.00 1.00 DW 1.00 1.00 | Legal | | 3.3 Permit Load R | ating | | | | |
| Temperature 1.00 | DW 1.00 1.00 * | | Lload Demand | 3.3 Permit Con Stress Ratio (0 | Silvery | | | | |
| T. Gradient 1.00 | T. Gradient 1.00 | Where, Capacity - De | Demand | | | FX-MIN | | Applied Stress | Stress R |
| Secondary 1.00 | Secondary 1.00 | R.F = Live Load | Dellie | Concurrent force | ein | Rebar Al | llowable Stress | (ks1) | 2.61 |
| Permanent 1.00 User Defined 1.00 | Permanent 1.00 User Defined 1.00 | Str | ain | | cracked | Tendon | (ksi) 1378.952 | 527.412 | 2,02 |
| * | * | Measure Type : St. Comp. | $\varepsilon_c / \Delta_c(in) = \varepsilon_t$ | Lcom / | Uncracked / Cracked | Tendon | 1378.952 | | |
| | | Lcom / Tens. | | Permit | Cracked | | | | |
| | | Comp. | 0.000E+00 1 0.000E+00 1 | | | | | | |
| · · · · · · · · · · · · · · · · · · · | | Legal Tens. | 0.0002.00 | Where, | Allowable Stress | 2 | | | |
| Live Load Combination | Live Load Combination | | | Stress Ratio = | Applied Stress | | mont | | |
| Live Load Factors for Rating | Live Load Factors for Rating | in which : | ated strain (displ | Calculate mome | ants in excess of | f cracking m | kip-ft | : Cracked | |
| Primary Vehicle Case(MV) v 1 | Primary Vehide MVL 1(MV) v 1 | $\varepsilon_{c}(\Delta_{c})$: maximum conce | | Calculate mom | | f cracking m -381420.87 | | | |
| Adjacent Vehicle Case(MV) V 1 | | $K = 1 + K_0 \times K_0$ | | Moead + IVILIVE | | | kip-ft | | |
| | Adjacent Vehicle MVL 1(MV) V 0 | $K_s = \frac{\varepsilon_o}{\varepsilon_s} - 1$ | | Wherey | $M_{\text{Dead}} = -0$ $M_{\text{Uve}} = -0$ | 0.022951786 | 5 kip-ft | | |
| Evaluation Live Load Model | Evaluation Live Load Model | | | | $M_{\text{Dead}} = -0$ $M_{\text{Live}} = 4$ | 3094785195 | S KIP | | |
| Design Live Load O Legal Load / Permit Load | Design Live Load Cegal Load Permit Load | | 1 | | | | | | |
| | | | | Section Propert | ties for the crack | ed section | 15.53045483 | in ³ | |
| Name of Rating Case | Name of Rating Case Design | | - | Section Propert | pth, c | = | 15.53045405 572170.8574 | | |
| Description | Description | | | Neutral axis de Second momen | t of inertia, ici | | don | | |
| Name Limit State Description | | | | Applied stress i | the reinforcer | nenter | 00111 | | |
| | Name Limit State Description | | | Applied stress | | 936.250 | 2549 ksi | | |
| Add | Design Service Add | | | - Tendon Effective pr | restress = | | 0901 5 | | |
| Modify | Permit Service Modify | | | aunace due | to Minear | | | | |
| | | | | Stress due t | to Milive = | -204.419 | 0740 | alose to 0.0 | |
| Delete | C Delete | | | Stress due Total stress | | that live loa | d demand valu | e is close to | |
| | | | | where "-" in r | esult table means | | | | |
| Close | Close | | | • Where | | | | | |

8. Traffic Load AK, N11 Update to Russia Standard

• The reliability factor for the UDL of AK vehicle load has changed from 1.15 to 1.25 to the latest amendments to SP 35.13330.2011.

Load > Moving Load > Vehicle

| tandard Name | Dynamic Factor | | | |
|---|--|--------------------------------------|------------------------|-------------------------|
| Russia - Road Bridge and Railway Bridge 🛛 🗸 🗸 | O Auto Calculation | - SNIP | | |
| ehicular Load Properties | Material Type RC | | | |
| /ehicular Load Name : AK | Bridge Type | Road and Town Bridge | | |
| Vehicular Load Type : AK ~ | Dynamic Factor (| (+Mu) | 1+(45-lambda |)/135 |
| | • User Input | | | |
| (Unit : KN) | Dynamic Factor (1+Mu) for Bogie | | | 1.4 |
| $P_1=10K$ $P_2=10K$ | Dynamic Factor (1+Mu) for UDL | | | 1 |
| | Load Reliability Factor O Auto Calculation O User Input | | | |
| D1 I K I4 1 10K 1.5 | O Auto Calculation | - SNIP actor (Gamm | | 1.5 1.25 |
| D1 I K I4 No Load(kN) Spacing(m) K 14 1 10K 1.5 2 10K end | Auto Calculation User Input Load Reliability F | - SNIP actor (Gamm | | |
| No Load(kN) Spacing(m) K 14 1 10K 1.5 2 10K end | Auto Calculation User Input Load Reliability F Load Reliability F | - SNIP actor (Gamm actor (Gamm | a f) for UDL | 1.25 |
| D1 I K I4 No Load(kN) Spacing(m) K 14 1 10K 1.5 2 10K end | Auto Calculation User Input Load Reliability F Load Reliability F Lane Factor (s1) | - SNIP actor (Gamm actor (Gamm | a f) for UDL Lane 2 | 1.25 Lane 3 and more |



8. Traffic Load AK, N11 Update to Russia Standard

- The axle load of N11 has changed from 14 K (14 x 11 = 154 kN) to 196 kN to the latest amendments to SP 35.13330.2011.
- N11 (2nd Edition) vehicle has been added.
- Load > Moving Load > Vehicle

| Standard Name | | | | |
|--|---|-------------------|------------------|--|
| Russia - Road Bridge and Railway Bridge | Consider the Effect of Tv | vo Vehicles as we | ll as One Vehide | |
| /ehicular Load Properties | Reduction Factor | | 0.75 | |
| Vehicular Load Name : N11(2nd edition) | Dynamic Factor | | | |
| Vehicular Load Type : N11(2nd edition) | V O Auto Calculation | | | |
| | Material Type RC | | | |
| | Bridge Type Rai | road Bridge, Sub | way, Tram | |
| P1 P2 P3 P4 | Dynamic Factor (1+Mu |) 1+10/ | (20+lambda) | |
| | User Input | | | |
| | Dynamic Factor (1+Mu |) | 1 | |
| | | 20 | | |
| < > < > < > D1 D2 D3 | | | | |
| < > < > < > D1 D2 D3 | Load Reliability Factor | | | |
| No Load(kN) Spacing(m) | Load Reliability Factor | | | |
| No Load(kN) Spacing(m) 1 196 1.2 | | | | |
| No Load(kN) Spacing(m) 1 196 1.2 2 196 1.2 | O Auto Calculation | (Gamma f) | 1,1 | |
| No Load(kN) Spacing(m) 1 196 1.2 | Auto Calculation O User Input | (Gamma f) | 1,1 | |
| No Load(kN) Spacing(m) 1 196 1.2 2 196 1.2 | Auto Calculation O User Input | | 0.8 | |
| No Load(kN) Spacing(m) 1 196 1.2 2 196 1.2 | Auto Calculation User Input Load Reliability Factor | | | |

9. Longitudinal Stiffener Input Measured from Bottom of Steel Composite Girder

- Longitudinal stiffeners can be defined with respect to the bottom of the steel beam. Previously, the distance was measured only from the top surface.
- This would be useful when you add longitudinal stiffeners for the tapered girders.

